LOWER BITUMINOUS MIXING TEMPERATURES

> REPORT 78-7 MARCH 1978

STATE OF VERMONT AGENCY OF TRANSPORTATION MATERIALS DIVISION

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Materials Division Highway Department Agency of Transportation March 27, 1978

Reviewed By: R. F. Nicholson, P.E., Materials Engineer

Date: March 31, 1978_

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HD 565 7/77	Prepared By: R. Snow Date: 7/22/77 Sheet 1, of 3
Vermont Department of Highways Materials Division - Research & Development Sub	division
RESEARCH INVESTIGATION	
Work Plan No. 77-R-55	
Subject Lower Bituminous Mixing Temperatures	
Investigation Requested By FHWA Letter Barrows to Crisman	Date June 13, 1977
Date Information Required Whenever a suitable project can be for	und
Purpose of Investigation In an effort to save energy (dryer fu	el), reduce mix temperatures
in 10° to 15° increments without sacrificing the quality cha	aracteristics of density,
coating and smoothness.	
Proposed Tests (Attach extra sheet if necessary) See attached	sheets 2 & 3 from FHWA
Notice N 5080.52 dated June 9, 1976. Project selected is	Ryegate Barnet I 91-2 (27)
Stage II.	
Proposal Discussed With Murphy Bartlett Willey	
Projected Manpower Requirements 9 man days (2 each plant & re	oad, 5 lab Willey)
Investigation To Be Conducted By L. Willey, Materials	
Proposed Starting Date Aug. 1977 Estimated Com	pletion Date Aug. 1977
Approval/Disapproval by Materials Engineer	Bon 8/9/77
Comments by Materials Engineer Approvality	aven only with
assumption that Contractors agreed	= otherwije
Highway Department denied and the	schore necestary
Agency of Transportation July 27, 1977 to Select Q	different project

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ABSTRACT

On September 8, 1977, a study of the effects of lowering the mixing temperature of bituminous concrete was performed on Interstate 91, Ryegate-Barnet I 91-2 (27) Stage II. The area studied was on the southbound lane from Station 693+25 (mile marker 115.932) to station 631+00 (mile marker 114.751).

Properties of the mix which appeared to be affected to the greatest degree were particle coating and compaction. A 15° F drop in mixing temperature, from 275° F to 260° F, was achieved before any apparent harm was done to the mix.

Although the values contained in this report are not representative of all possible paving situations, the findings are indicative of what can reasonably be expected.

INTRODUCTION

The primary objective of this study is to determine the lowest possible mixing temperature of bituminous concrete, under normal operating conditions, without sacrificing the quality of the finished pavement.

In June 1977, the F.H.W.A. office in Montpelier contacted the State of Vermont, Agency of Transportation, Materials Division, regarding the subject of "Lower Bituminous Mixing Temperatures". It was the intent to study what effect lowering the mixing temperature of bituminous concrete would have on pavement physical properties and performance.

Therefore, this study was undertaken in the interest of conserving energy (less fuel required for lower mixing temperatures) and possibly increasing pavement life (asphalt cement binder retains its life better, at lower mixing temperatures).

The project chosen for this study was on Interstate 91, Ryegate-Barnet I 91-2 (27) Stage II. Type II, 3/4" binder mix, was monitored. See Figure 1.

MATERIALS

Type II bituminous concrete, 3/4" binder mix, was used as the wearing course for Stage II construction on this project.

The coarse aggregate used was crushed stone from L. M. Pike's quarry in Ryegate, Vermont. Fine aggregate consisted of a blend of crusher dust from L. M. Pike's quarry and natural sand from Calkins of St. Johnsbury, Vermont. The asphalt cement was a 150-200 penetration grade asphalt from Gulf of Montreal, Quebec, Canada.

The "Mix Design" for the Type II mix and a "Temperature-Viscosity Chart" for the asphalt cement are contained in Appendix C.

The 150-200 penetration grade asphalt cement, being a soft grade of asphalt, requires lower mixing temperatures than the stiffer grades of asphalt. Therefore, a drop in mixing temperature of approximately 10° F is possible, simply by using the softer asphalts.

PROCEDURE

The general approach of this study follows guidelines as outlined in the F.H.W.A. Notice N 5080.52, dated June 9, 1976. The intent being to lower the mixing temperature of bituminous concrete by gradual increments $(10^{\circ} \text{ F to } 15^{\circ} \text{ F})$ until such time as the physical properties of the mix are detrimentally affected.

The study was carried out September 8, 1977. Ambient project temperature was on the rise, ranging from 67° F to 76° F. The weather was clear, with a light breeze.

A state inspector at the plant monitored such items as raw aggregate moisture content, dried aggregate moisture content, ambient plant air temperature, temperature of the discharged mix, and ross count (particle coating) of the mix.

Project observations included monitoring ambient air temperature, haul length and time, mix lay down temperature, uncompacted mix depth, and numbers and types of pavers and rollers.

Percent air voids of the compacted mix, for each temperature interval, was determined from the plant quality control records and from tests done on special request. These tests were performed in accordance with the Marshall Method.

Compaction achieved relative to target density was determined, for each temperature interval, using a nuclear density gauge. Two sets of tests were run to determine compaction. The first set being quality control tests which are normally run as a basis for payment. The second set was run on special request as part of this study.

Pavement roughness was measured using a May's Ride Meter for the entire day's production. Roughness for each temperature interval was also determined.

RESULTS

Air Voids of Compacted Mixture as Determined by Marshall Method (Figure 2)

As the mixing temperature was lowered, the percent air voids increased slightly. However, for mixing temperatures ranging from 275° F to 240° F, there did not appear to be any difficulty in achieving the required level of air voids. i.e. 2% to 5%.

Ross Count (Figure 3)

As the mixing temperature was lowered, the stone particles remained 100 percent coated, down to a temperature of 265° F. At least 95% of the particles remained coated down to 235° F. However, for temperatures below 250° F, the sand particles in the mix did not appear to be thoroughly coated.

Compaction Achieved Relative to Target Density (Figure 4)

The quality control tests indicated that compaction failed around 270° F and continued to decline as the temperature was lowered. However, the special request tests indicated compaction failure occurred at around 260° F. Below 260° F, down to 240° F, percent compaction remained fairly constant at around 97.8%. Surface Characteristics - Roughness (Figure 5)

Pavement roughness was 42.2 inches/mile at a mixing temperature of 275° F, but decreased to an acceptable level for lower temperatures, down to 250° F. In the section paved at 240° F, the roughness jumped to 58.9 inches/mile. This may be due in part to the fact that this section was at the end of the day's production.

CONCLUSIONS

Properties of bituminous concrete that appeared to be detrimentally affected by lowering the mixing temperature, within the temperature range studied, were particle coating and compaction.

Particle coating became critical at 240° F, with the sand portion of the mix appearing partially coated below 250° F.

Compaction achieved relative to target density, on the tests run for this study, fell below acceptance limits for temperatures below 260° F.

Thus under the given conditions, a 15° F drop in mixing temperature, from 275° F to 260° F, was possible without harmfully affecting the finished pavement. Remedial measures such as longer mixing time and greater compactive effort might enable the mixing temperature to be lowered even further.

Values contained in this report are not representative of all possible paving situations. However, the established trends are indicative of what can reasonably be expected by lowering the mixing temperature of bituminous concrete.

Vermont Agency of Transportation Lower Bituminous Mixing Temperatures

Field Lab Information

1. Moisture Content of Raw Aggregates:

Raw Date/Time Aggregate	9/8/77 11:00 AM	PM	AM	РМ
3/4"	0.14 %			
1/2"	0.25%			
3/8"	0.24%			
Sand	3.07%			
Dust	1.86 %			

2. Ambient Air Temperatures:

Date <u>Sep</u>	tember 8, 1977	
Time	Temperature	
6 A.M.		
7		
8		
9		
10:30	62 ° F	
11	66 °F	
12	72° F	
1 P.M.	74°F	
2	74 ° F	
3		
4		
5		
6		

Date	
Time	Temperature
6 A.M.	
7	
8	
9	
10	
11	
12	
1 P.M.	
2	
3	
4	
5	
6	

Field Lab Information

3. Temperature and Moisture Content of Dried Aggregates:

	Date	Septer	nber	8,19	77		Date	0.000 + + 0.000 + + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0.000 - + 0	anaan marana ay waxaa ma			and training
Bin	A.M. Time	Temp.	⊁ % H20	P.M. Time	Temp.	* % H20	<u>A.M.</u> Time	Temp.	% H20	P.M. Time	Temp.	% H20
S	11:50	275	0	1:24	250	0.17						
2				2:01	260	0.20						
3					-							
4												

* Moisture Sam ples obtained from Hot Elevator Discharge Chute. 4. Temperature of Mix as Discharged From Mixer:

Date	9/8/17		Date	9/8/77		Date	9/8/77		Date_	9/8/77	
Time	Slip #	Temp.	Time	Slip #	Temp.	Time	Slip #	Temp.	Time	Slip #	Temp.
10:18	47042	280		47059	275	12:17	47074	270	1:47	47101	245
	47043	290		47060	275		47075	260		(Drop To toz40	emP)
	47044	285		47061	265	12:41	47081		1:54		240
10:28	47045	275		(Plant d			47082		equilibre 4	(Marshall	c5 235
10.20	47046	275		470 6Z	290	12:50	(Drop To to 250	2mp.)	~ ~ 1	47106	240
				,							z45
10.45	47047	275		470.63	250	12.54	47085	255	214	47107	
10.43	470 50	270		47064	265		47086		2.14	47109	240
	470 51	275		470.65	265		<u>470B7</u> (Te5+)	260		47110	240
	47052	275		47066	260	 	47088	260		47111	250
	470.53	275		47067	265		47089 (Loads	255 not)		47.112	240
-	47054 rmed co	280		47068	265		Covere	9)		47113	240
	op Temp			47069	265		47091	250		(Last Load 47114	240
11:02	47055	275		47070	265		47092	255			
	47056	275		Marshall 47071	A) 265		47093	255			
	470 57	2.70	12:09	47072	255	1:24	(Marshall 47094	B) 250			
	47058	270		47073	255	1:31	47096	255			

APPENDIX A

Field Lab Information

5. Ross Count of Mixture:

Date	Time	Slip #	Temperature	% Coated Particles
9/8/77	10:30	47047	275 °F	100
	12:47	47082	265 °F	100
generalises in the construction of the construction of the con-	1:10	47089	255 °F	98
an an air air an	2:01	47105	235 °F	95
[Visual	examinat	ion of trucks	showed sand)
				emperatures
	below	250°F.		

APPENDIX A

Project Information (Ryegate-Barnet I 91-2(27) S/2)

1. Ambient Air Temperatures:

Date <u>Sep</u>	tember 8, 1977	Date
Time	Temperature	Time Temperature
6 A.M.	, 	6 A.M.
7		7
8		8
9		9
10		10
11	67 °F	
12	72 °F	12
1 P.M.	74°F	1 P.M.
2	75°F	2
3	76°F	3
4		4
5		5
6		6

2. Length and Time of Haul (Average):

Temperature Interval	Miles Length	<u>Minutes</u> Time
275 °F	o.8	5
260 °F	0.6	5
250 °F	0.4	4
240°F	0.3	4

Project Information (Ryegate-Barnet I 91-2(27) S/2)

3. Factors Affecting Laydown and Compaction:

Paver Type(s) <u>Mainline</u>: (1) <u>Blaw-Knox PF220</u> <u>Right Shoulder</u>: (1) <u>Blaw-Knox PF180H</u> Roller Type(s) (2) <u>Galion-2Axle tandem Steel drum Rollers</u> (1) <u>Bros. Pneumatic tired roller</u>.

(1) Galion - 3 Axle tandem Steel drum roller.

Mix Arriving At Project

Date	Septemb	er 8, 19	77		Date	Septem	ber 8, 19	776	
Time	Slip #	<u>3.B.</u> <u>M.P.</u> (Station)	(°F) Mix Temp.	Uncompacted Depth. (in.)	Time	Slip #	$\frac{5.B.}{M.P.}$	(F)Mix Temp.	Unc. Depth
11:12	47055	658400	275	21/8	1:35	47095	641100	250	z1/8
11:20	47056	657+50	275	21/8	1:41	47096	640+50	250	248
11:24	470 58	657+00	270	2 1/4	1:50	47099	639+00	245	2/8
_11:29	47060	656400	275	2	1:54	47100	638100	250	2
11:45	47062	655+50	265	21/8	2:04	47103	637+00	245	2 1/8
11:51	47063	655+00	265	21/8	2:11	47105	636400	240	2/4
11:55	47065	654+00	265	2.14	2:15	47106	635+50	245	21/8
12:04	47067	653+50	2.65	21/8	2:18	47107	635+00	240	2/8
12:11	47069	652,+50	270	21/8	2:24	47109	634100	240	21/4
12:15	47070	652+00	2.65	218	2:42	(Last Load) 47114	631+50	240	21/4
12:19	47071	651+50	265	21/4	- End	at Sta	631700	etilitiireaanae -	
12:25	47072	651+00	265	21/8					
1:02	47084	645+50	260	21/8	<u></u>	<u> </u>			
1:08	47086	645+00	255	214	<u></u>		6		
1:12	470 87	644+00	255	21/8	Constant and the second se	a a gun an a Barr Da a dha a dh' Agun a Bh' a Barr Dan dhan An			
1:20	47089	643+50	255	2.14					
1:23	47090	643100	260	2.14	ter-fundersämilitersternitern		0-113		
1:28	47092	642+00	2.50	2.48		. <u></u>	9	, t	. .
1:31	47093	641+50	250	21/4	10-11-10-10-10-10-10-10-10-10-10-10-10-1				-

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.D7	30	н	#16	33.6	32.0	326	34.2	301	33.6	33.7	32.3	31.9	313
D8	24	11	#30	25.3	245	29.8	25.4	21.9	26.8	27.2	26.0	25.0	22.9
D9	15	11	#50	15.9	15.3	15.7	15.7	13.4	17.1	17.4	176	15.2	13.7
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G	S/(S+F)	" – F	illed	1.89	72.3	11.2-	82.6	79.2	86.3	76.0	78.8	76.1	76.3
Н	P x 62.4	Unit Wgt.,1	bs/ft3	154.8	152.9	151.6	154.3	154.4	156.0	153:1	154.0	1543	154.1
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M		Wgt. in Wat		746	767	720	782	773		753			810
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	APPENDIX A											
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E		Bitumen % (AC)	5.50	5.39	5.28	-	1					
F	100(R-P)/R	% Voids - Mix	. 2.2	3.1	3.8							
G.	S/(S+F)	" - Filled	84.0	80.9	77.4	1				N		
H	P x 62.4	Unit Wgt., 1bs/ft3	155.4									
·I		Stab conv.,1b.		1188	992							
J		Marshall Flow Valu		6.	6							
						Ter	mp					
K		Sample Thickness,	$n. 2^{3}/8$	2/16	2%							
'L		Wgt. in Air, grams			1160							
M		Wgt. in Water, gram			688							
N	L - M	Volume, cubic cm.		444		· · ·						
P	L/N	Sp. Gr Bulk	2,491	2:473	2,458							
R	Sce below	Sp. Gr Theor.	2.546									
S												
T	· · · · · · · · · · · · · · · · · · ·	Stab measured,1					t					
U		Accepted or Reject		47094	47105	-54	P-1					
Th	eoretical S	pecific Gravity Fo	rmula:						I	nspect	tor(s)	
	100 ÷ ($\frac{\%AC}{Gr. AC} + \frac{\% + 8}{Sp}$	(100%-%A	c) +	% - 8	3(100%-	-%AC)	-)	E	BI	odget	T _
	Sp.	Gr. AC Sp	. Gr. +8		SI). Gr.	-8				•	
-	13											

9-8-77 W CHKD. BY____DATE

APPENDIX A COMPACTION - 5B

SHEET 5 OF 7 NOB NO. I.91-2 (27) IL Rugate - Barnet

$\begin{array}{c c c c c c c c c c c c c c c c c c c $	Fill Gall & Row and Barry appear		affingenner – den e han antrese av skærne virkning som af ble destarder av s				4	T. 5. =	147.2
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	Salaranda Hospitala	Vest	Station	off.			Den. (Chart)	test steam tog a same tagter spep-	
A.M. 3. $(690+00)$ 4. (619) 318 148 100.5 1940 4. $(686+00)$ 11.2' 625 32.1 147 99.8 1957 5. $(686+00)$ 11.2' 605 337 142 96.4 1940 7. $(686+00)$ 4.2' 646 332 143 97.1 1940 7. $(680+00)$ 4. (448) 333 143 97.1 1953 9. $(72+00)$ 4. (428) 333 143 97.1 1953 9. $(72+00)$ 4. (428) 332 143 97.1 1953 9. $(72+00)$ 4. (429) 32.3 146 97.1 1953 9. $(72+00)$ 4. (429) 32.3 146 97.1 100.5 12. $(674+00)$ 4. (420) 319 148 100.5 12. $(660+00)$ 4. (620) 32.0 136.5 92.7 12. $(72+00)$ 8. (31) 6. (600) 318 148 100.5 12. $(666+00)$ 4. (643) 330 143.5 97.4 13. $(666+00)$ 4. (633) 350 136.5 97.4 14. $(666+00)$ 4. (633) 351 130 92.3 14. $(72+0)$ 8. $(660+00)$ 4. (633) 351 130 92.3 14. $(72+0)$ 8. $(660+00)$ 4. (633) 322 144.5 97.8 50 851 850 14. $(662+00)$ 4. (633) 322 143 97.1 17. $(660+00)$ 4. (633) 332 143 97.1 18. $(25+00)$ 4. (613) 332 143 97.1 11. $(76+26)$ 18. $(25+00)$ 4. (613) 332 143 97.1 11. $(76+26)$ 18. $(26+00)$ 4. (26) 332 143 97.1 10. $(72+10)$ 8. (26) 13. (26) 4. (26) 332 143 97.1 14. $(27-10)$ 8. (26) 4. (26) 332 143 97.1 14. $(27-10)$ 8. (26) 4. (26) 332 143 97.1 14. (26) 9. (26) 4. (26) 332 143 97.1 14. (26) 4. (26) 332 143 97.1 14. $(27-10)$ (26) 4. (26) 332 143 97.1 14. $(27-10)$ (26) 4. (26) 332 143 97.1 14. $(27-10)$ (26) 4. $(27-1)$ 342 138.5 94.0 14. $(27-1)$ (26) (26) 4. $(27-1)$ 342 138.5 94.0 15. (26) 4. $(27-1)$ 342 138.5 94.0 16. $(27-1)$ 342 138.5 94.0 17. (26) (26) 4.00 4. (26) 329 141 95.7 14. $(27-10)$ (26) (26) 4. $(27-1)$ 342 138.5 94.0 14. $(27-1)$ $(27-10)$ (26) $(27-1)$ (26) (26) $(27-1)$ (26) $(27-1)$ $(27-$		/	692+00	E	617	317	148		693+25
$\begin{array}{c c c c c c c c c c c c c c c c c c c $. 1	2.	690+00	4	619	_318	148		e contractor a 1 - por a su por second por la participa na administra de materio a
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	A.M.	3	688+00	11.2'		321	147	- 99.8	erer haat maa milan di art i waxa mini ana pian asati kutur ta
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$			686+00	Lt.2'		313	150		
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	194'	5	684+00	R1.2'	655		142	96.4	a demonstrating particular to the same of data speculation constrained and
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1951		682+00	R1.2'		332			an a
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1940		680+00	E		333	143 .		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1030		678+00				14-3	97.1	
$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	14.22	9_	676+60	4.31		319	148	100.5	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	200	10		4.3'		323	146		
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1945,2	11		Rt.3'	680		136.5	92.7	*
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	5	12		Rt. 3'		318	148	100.5	
$\begin{array}{cccccccccccccccccccccccccccccccccccc$		13		E			143.5		A to de la companya de la
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	275° ±	11				336	142		andentral discrimination remaining a distribution
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	98.0%	15		1			136		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	1010 10						144.5		50 REST AREA
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	and a second			R1.41					0
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				R1.4'			143	97.1	TEMP. 2450
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	98.8%			E	618		148		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		deletingersons		E			140.5		A Description of the second
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	260°			E					Begin P. M.
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				and a second sec					
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$,	1				96.4	
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	oNo					-			
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	10	25							TEMP TO 250
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	055250	26		Kt.2			1 1		
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	- n10 *							99.5	
q123 32 13,7 13,7 13,7 33 34 10,1 10,7 0,1,400 35 36 10,1 10,7 37 33 10,1 10,7 38 37 10,7 10,7 39 10,7 10,7 10,7 40 10,7 10,7 10,7	965000	28	638+00	a property and the second data where			1		TEMO TO ZANO
q123 32 13,7 13,7 13,7 33 34 10,1 10,7 0,1,400 35 36 10,1 10,7 37 33 10,1 10,7 38 37 10,7 10,7 39 10,7 10,7 10,7 40 10,7 10,7 10,7	1934 00	29	636+00	E					
q123 32 13,7 13,7 13,7 33 34 10,1 10,7 0,1,400 35 36 10,1 10,7 37 33 10,1 10,7 38 37 10,7 10,7 39 10,7 10,7 10,7 40 10,7 10,7 10,7	95 mm	30	634+00	E					END MANNG
35 36 37 33 39 39 40 36	123-	31	632+00	L_L_	604	334	141	95.7	631+00
35 36 37 33 39 39 40 36	9.04.6	32							
35 36 37 33 39 39 40 36	5= 147	33		· · · · · · · · · · · · · · · · · · ·					
36 37 37 NECEIVED 33 SEP 15 1977 39 MUMWAY 40 SEP 1.5		39			South				ang desetted the back and a second second second second second
37 33 39 40 NECEIVEU SUP 15 1977 197					1 Aller	×			
33 39 40				A	Y RECEIVEN	8			
39 10 10				·	1				
10						5			
					STIET. LAB	£7		•	
Sum of % Compaction 3005.8 = 31		90]	PIGITIE!	ý/	L		

Sum of % Compaction 3005.8 = 31

Record Standard Counts on the back of this sheet. For additional tests, use additional sheet.

14

OF MATERIAL DIVISION TEMPETURE TEST RUN THIS DATE

Pay Factor .O

Average % Compaction _ 96.9676

STATIONS 631400 - 655+00 WILL NOT BE Q.C. BECAUSE

Form 3

TO: LARRY WILLEY, MATERIALS DIVISION FROM: WALKER, CONSTRUCTION DATE: 9-12-77 SUBJECT: RVEGATE - BARNET II 91-2 (27) II SOUTH BOUND LANE Per your request the following information was obtained, using the Probe, at the stations you listed, after The 3 axle roller had finished: STATION OFFSET COUNT RATIO DEN. (CHART) & COMPACT REMARKS											
	STATION	OFFSET	COUNT	RATIO	DEN. (CHART)	% Compact	REMARKS				
	658+00	Q	621	315	149	101.2	START LOUGR				
	658+00		632	320	147.5	100.2					
275°	658+00		639	324	145.5	98.8					
	656+00		618	313	150	101.9	(275° - 100.1%)				
	656+00	Lt. 4'	629	319	148	100.5					
	656+00		648	328	144.5	98.1	1				
	654+00	E	640	324	145.5	98.8					
	654+00	Lt. 2'	645	327	145	98.5	2				
260°	652+00	£	650	329	144	97.8	(260° - 98.1%)				
	652+00	Rt. 61	658	333	143	97.1					
۹.	644+00	E	649	329	144	97.8					
L	644+00	H. 3'	641	325	145	98.5	TEMP. TO				
250°	641+00	E	655	332	143	97.1	250° AT 642+00± (250°-97 8%)				
	641+00	Rt. 31	644	326	145	98.5	(250° - 97.8%)				
240°	635+00	E	652	330	143.5	97.4	240° AT 636+00±				
	635+00 ht. 6' 651 330 143.5 97.4 (240°-97.8%)										
	632+00	E	643	326	145	98.5	1				
	* St	ANDARD (POUNT =	1974	TEST STR	eip = 147	7.2 -*				

-]	APPENDIX A	1 Annual 1		in the second
C t t	- May: 5 Mete	Rus	58 613725	CAT NO IUJS RECUERE
			2 Jan	
		M.M. HAL MAN		AUSTIN, TEXAS 78751
		HANNYMYAYMANA		RAINHART CO.
		144 MAN AN AN AN AN		(C) 1969
	215° 0.038		E.1 "	
	260° 2 0.2416 0	1 Martin Contraction of the second se		
		Myrth hurth When		• • • •
- I I I I	240° 250° 0.114 0.114 <i>Lun #</i> 1 <i>Nov. 10, 1</i> 47	WWWWWW / WWW		
		Mummin / /m	58 631400	
	TEMR-	MINY AND A MARKA		r. NIED IN
	1 1 1 1 1 1	6		

(May .< Ma	eter WWW	42	5.8.631400
0,114		1. 1. 1 	
260°	Arthony Arthony Arthony	1/2.2.2	212
215°	AV MARINA ANALY		5.8.658400
			21
	1		
Eun #2.			125
			1 2B 693425
MILES=	луничник, Момомодология и торого умуницини и торого и тор		

APPENDIX A May's Met		~ # 3	5B693+25	
TEMP.= 240° 250° 260° 215 MILES= 0.114 0.114 0.246 0.038 Lun #3 Mon, N, 1977		12.2 7.2 1.2 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	5B631400 58 659:00	2014
18	יין איזיילי איזיאיזאיזאיזאיזאין איזיאע אואיזאיזאיזאיזאיזאיזאיזאיזאיזאיזאיזאיזאיזא			

	(⁰ F)				(⁰ F)	
Slip #	Temp.	QC/SR	% Air Voids	Station	Temp. Interval	Ave. % Air Voids
46969	275	QC	3.3		275±	4.3
47003	280	QC	4.6			
17020	200	00	5 0			
47028	280	QC	5.0			
47071	265	SR	2.2	651+50	260	2.8
11 01 0						-
47072	260	QC	2.8	651+00		
47088	260	QC	3.3	644+00		
17001	050	0.5	0.1	(11:00	250	0.1
47094	250	SR	3.1	641+00	250	3.1
47105	240	SR	3.8	636+00	240	3.8
					•	

Compaction

(^O F) Temp. Interval	Station	QC/SR	Ave. % Compaction	Composite Ave. % Compaction
275±	692+00 - 658+00	QC	98.0	98.0
275	658+00 - 656+00	QC SR	98.8 100.1	99.5
260	656+00 - 643+00	QC SR	96.1 98.1	97.1
250	643+00 - 637+00	QC SR	94.9 97.8	96.4
240	637+00 - 631+00	QC SR	93.6 97.8	95.7

QC: Tests performed under quality control program. SR: Tests done on special request.

APPENDIX B

Roughness

(^o F) Temp.	Station From To		(Miles) Length				0	(x6.4) Factor	(÷ Length) Inches/Mile-Roughness
240	631+00	637+00	0.114	1.06	0.84	1.20	1.05	6.72	58.9
250	637+00	643+00	0.114	0.48	0.66	0.60	0.58	3.71	32.5
260	643+00	656+00	0.246	1.46	1.64	0.96	1.35	8.64	35.1
275	656+00	658+00	0.038	0.40	0.26	0.32	0.33	2.11	55.5
275*	658+00	693+25	0.668	4.72	4.08	4.18	4.33	27.71	41.5
275**	656+00	693+25	0.705	5,12	4.34	4.50	4.65	29.76	42.2
Composite	631+00	693 + 25	1.179	8.12	7.50	7.28	7.63	48.83	41.4

*This section not monitored during paving.

**Includes sections paved at 275° F, monitored and not monitored during paving.

APPENDIX C STATE OF VERMONT

Design of Bituminous Concrete Mixtures

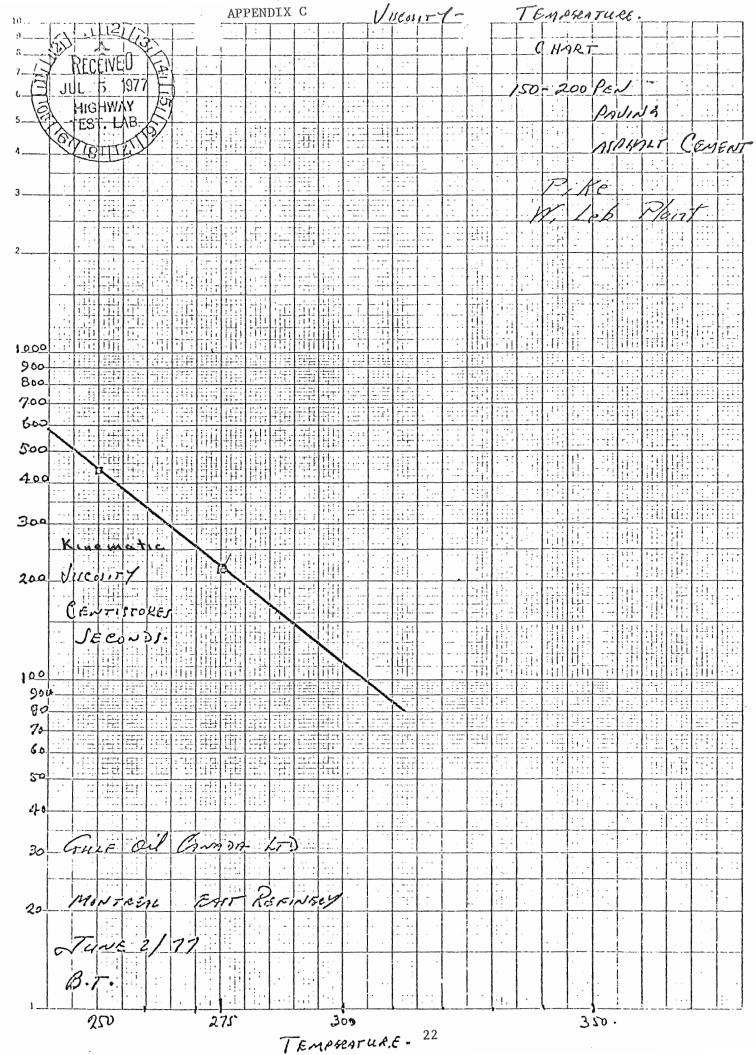
Town R/ECATE - BARMET Project No. Z-91-2(27) St.T.

422

No

Gentlemen:

In acc	ordance with	the spe	cificatio	on requi	rements	s for the	above 1	project	I submit	the foll	owing j	ob mix f	ormula:	ut-
Pavement	Туре 📿	e				Gradatio				Plant Lo	ocation.	17726 8	03	v
Size	% Used	1 13/	11/	1	1	1/2	3%8	I	8	16	30	50	200	1
SAHO	30	1%	11/2	1	3/4	100	96	90	82	70	64	29	5	
	15		1			100	100	98	76	52	360	26	13	
Dust ³ /E	22					100	94	29	8				/-	
1/2 3/4	5				100	98	25	4				1		
3/4	28			100	92	28	4							
Resultant	100		ļ	100	98	80	67	47	38	29	24	13	3.5	
Resultant	1 700		1	100						1 ~ /	127	175	12.3	<u> </u>
	······			п		Gradatio	n %	Passing						
Bin	% Used	1¾	1½	1	3⁄4	1/2	3%8	4	8	16	30	50	200	
S	43						1 11 1	100	84	67	53	30	8.1	
2	25						100	30	6					
3				-	1	100	26	4						1
<u> </u>	27				100	22								
Resultant	100			100	188	100	69	50	38;	29	23	13	3.5	
						79								
Batch	Bin S		Bin No.		Bin No	b. 3	Bin N		Bin	No. 5	-	AC	T	otal
Weights	4076		2370	>	474		256	,6			3	20	100	00
	1	1%	11/2	1	3/4	1/2	3%	4	8	16	30	50	200	AC
Job Mix		- /4	- 12						1	30				
Formula				100	98	80	68	48	38	50	24	15	4	5,2 .
Job Aim														
Specification Limits				100	95	74 88	62	44/12	30/48	20/38	13	8 22	2	5/11
					Sou	arce of 1	Material	S						
		Aggrega	ates							Aspl	nalt			
Coarse: P	INE - RYE						AC-5:							
	12 1-11	011112	¥/*				150-200 - GULF - CANADA							
Fine: Dos	t- PIKE.	- R130	SATE	vta			AC-10				1110/11	///	· · · · · · · · · · · · · · · · · · ·	
SAIN	0 - CALK	1N'S - 5	t. Jon	HNS BU	RY Y	te	<u> </u>							
							Other:							
Mixing Tim	Dry.	H		Wat.	. 34		Tota	. 4	0	Tor	manatu	ra. 2	75 = 20	>
	by: Ch		D H		- 1	,	10ta	•	- \	Iei		10	7	•••••
Submitted	by:	ucco	C	2017	ic	•••••••••••	(s	ignatur	e)	Date	: . <i>0</i>	£.£/./		
Company	PIKE	LND.	<u>LKCi</u>	-						(25,	••••••			
				FOR S	TATE (OF VER	RMONT	USE O	NLY		1			
	1	А	pprove	d		1	_	Reje	ected			á TÍI	112,	
Comments:	74	7.1. t	the and share the	J.J	L.K.C.K.d	C.C.C. P.A.		5	. A		· K	Jeres .		
	1.6.2.1.6	t.l., c	.1.7.7.67.6.	r.c.t.c.	2.1.1.1.1.1.	<i></i>						' RECE	IVED X	
				••••••••••••			·····					AUG 22	2 1977	14
	<i>i</i>			•••••••••••••••••••••••••••••••••••••••							. 9	HIGH	NAV I	E
Signature .			ilant.		Title	13.1		7	1.2.9.1		. 14	TEST.	LAB	57
HD 554 500 Du							Date	1. /	120	-	. %	Trom	119	<i>Y</i>
						21						Vall	いン	



46 5810 Made IN U.S. N. SEMI-LOGARITHMIC 3 CYCLES X 140 DIVISIONS KEUFFEL & ESSER CO.

	STATION	STUDY LOCATION:	FIGURE 1 I 91 SOUTHBOUND RYEGATE-BARNET I 91-2 (27) S/II PAVED SEPTEMBER 8, 1977 STA. 693+25 to STA. 631+00		
	693+25	Percent <u>Air Voids</u>	Ross Count	Percent Inches/Mile Compaction Roughness Q.C. S.R.	
Section : 275 ⁰ F: (Not Mon: - Contro)	<u>t</u>		100	98.0	
Section 2 275° F Section 3 260° F	658+00 — 656+00 —	2.8	100	98.8 100.1 55.5* 96.1* 98.1 35.1	
Section 4	643+00	3.1	98	94.9* 97.8* 32.5	
250 F Section 5 240 ⁰ F	637+00-	3.8	95	93.6* 97.8* 58.9*	
		23	S	.C Tests performed under Control Program .R Tests done on Special * - Test values outside acc limits.	Request.

